



# MARITIME FUSION

An Introduction: Low Power Density Tokamaks for Off Grid Applications

Presenter: Justin Cohen

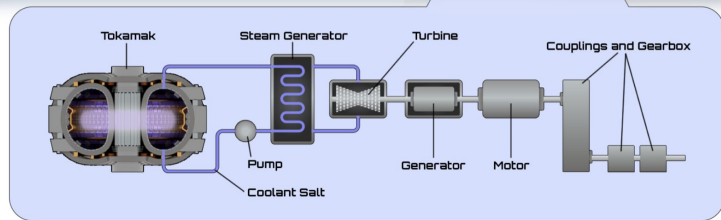


# Maritime Fusion: Past, Present, and Future

- Company launched via Y Combinator in early 2025
- Rough 0D reactor design
- Closed our seed round earlier this year
- Opened our HQ in San Francisco, grew headcount to 8



- Develop, manufacture, and test our HTS cable
- Publish a detailed physics basis
- Model the economically viable operations of fusion powered vessels
- Contractual obligations with customers



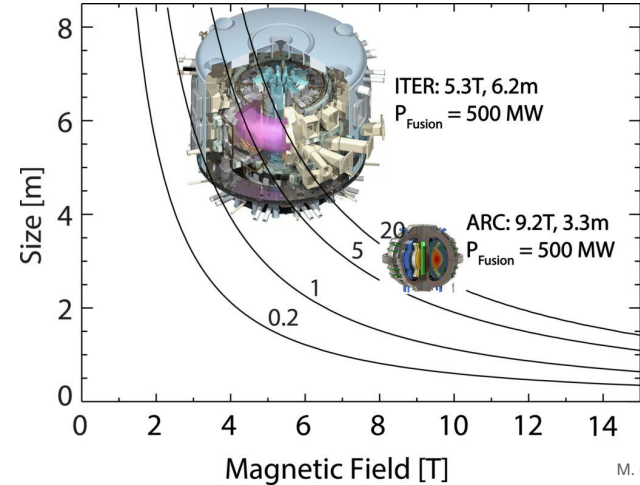
- No intermediate sized device, full scale Yinsen tokamak demonstrator 2032-2035



# WHY NOT THE GRID?

## The FOAKs Battle Against Material Science for Cost

Trade large expensive reactor that doesn't require any more Nobel prizes → smaller cheaper reactor that requires decades of innovation for commercial viability



M. Greenwald, 2019



Minimize Reactor  
Construction Cost

Compact and  
High Field

High Heat Flux,  
Mechanical  
Stresses, Activated  
Structures

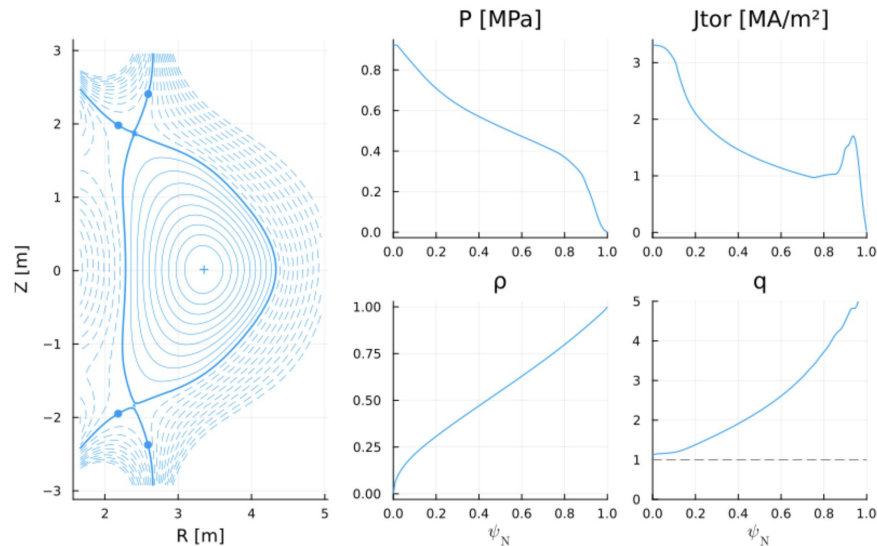
Low in Vessel  
Lifetimes,  
Maintenance  
Operations, Low  
Capacity Factor

**Not Competitive  
Power Source on  
the Grid**

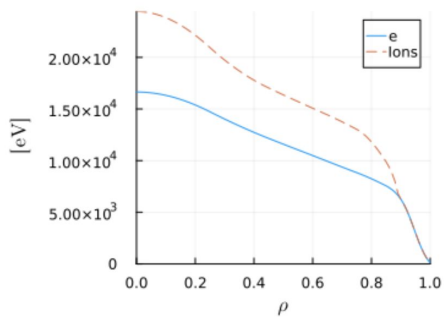


# Tokamak Design Point

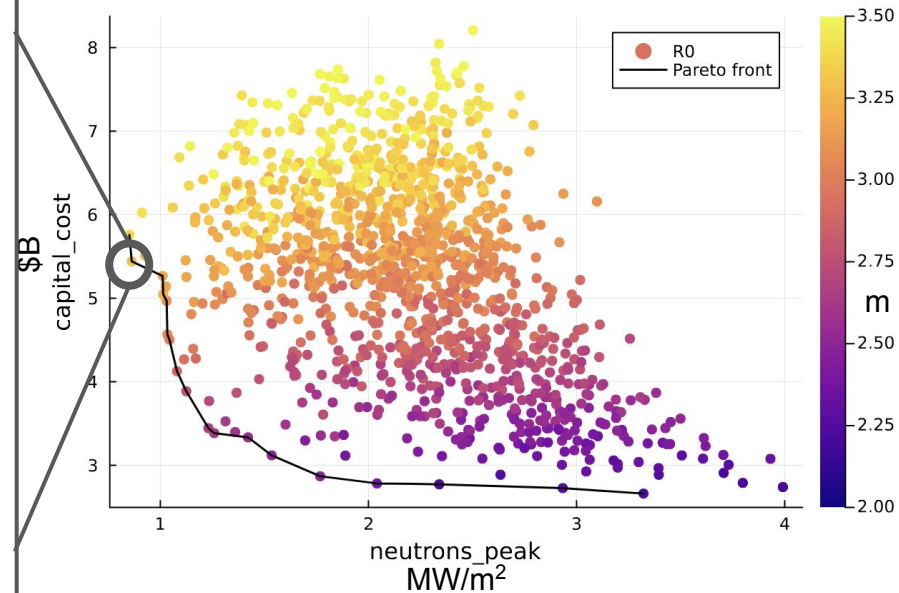
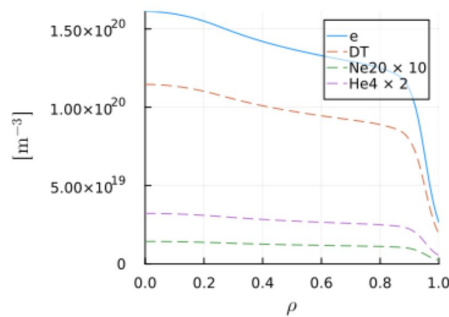
MARITIME FUSION



Temperatures



Densities



Each point in the plot is a fully resolved design  
- each with solutions for equilibrium, transport, HCD, etc...



# Resulting device is roughly JET-sized...

## GEOMETRY

**R0** → 3.31 [m]  
**a** → 1.02 [m]  
**1/ε** → 3.23  
**κ** → 1.82  
**δ** → 0.82  
**ζ** → -0.0155  
**Volume** → 106 [m<sup>3</sup>]  
**Surface** → 180 [m<sup>2</sup>]

JET R0: 2.96 m  
JET a: 1.25 m

## DENSITIES

**ne0** → 1.61e+20 [m<sup>-3</sup>]  
**ne\_ped** → 1.08e+20 [m<sup>-3</sup>]  
**ne\_line** → 1.37e+20 [m<sup>-3</sup>]  
**<ne>** → 1.24e+20 [m<sup>-3</sup>]  
**ne0/<ne>** → 1.3  
**fGW** → 0.602  
**zeff\_ped** → 2  
**<zeff>** → 2  
**impurities** → DT Ne20 He4

## EQUILIBRIUM

**B0** → 7.86 [T]  
**ip** → 7.51 [MA]  
**q95** → 4.85  
**<Bpol>** → 1 [T]  
**βpol\_MHD** → 1.11  
**βtor\_MHD** → 0.0179  
**βn\_MHD** → 1.97

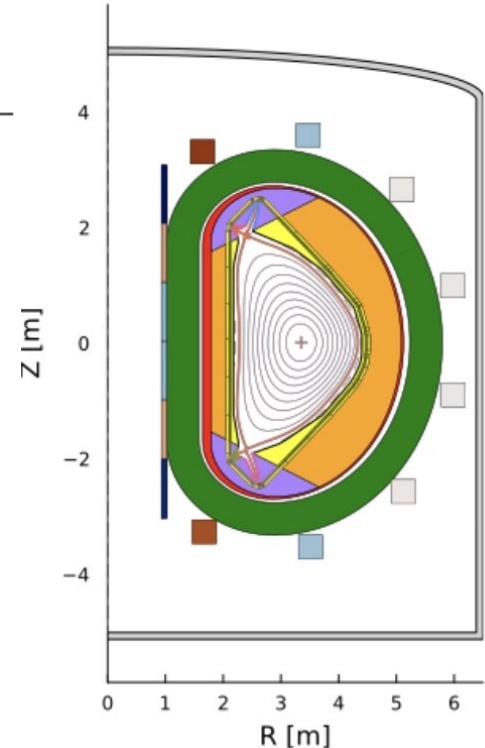
## PRESSURES

**P0** → 0.947 [MPa]  
**<P>** → 0.439 [MPa]  
**P0/<P>** → 2.16  
**βn** → 1.91  
**βn\_th** → 1.91

Operating at  
nearly twice  
JET's field and  
1.5x plasma  
current

## TEMPERATURES

**Te0** → 16.6 [keV]  
**Ti0** → 24.4 [keV]  
**<Te>** → 9.5 [keV]  
**<Ti>** → 13.2 [keV]  
**Te0/<Te>** → 1.75  
**Ti0/<Ti>** → 1.85





# But achieves a SPARC-like $P_{\text{fusion}}$ and 30+ MW net electric

Yinsen has an advantage over other devices in power handling with  $P_{\text{sol}} / R$  limited to **9.6 MW/m** in this case → 67% the ITER/DEMO limit of 15 MW/m!  
[1]

## SOURCES

**Pec** → NaN [MW]  
**rho0\_ec** → NaN [MW]  
**Pnbi** → NaN [MW]  
**Enbi1** → NaN [MeV]  
**Pic** → 7.66 [MW]  
**Plh** → NaN [MW]  
**Paux\_tot** → 7.66 [MW]  
**Pa** → 33.7 [MW]  
**Pohm** → 0.456 [MW]  
**Pheat** → 41.8 [MW]  
**Prad\_tot** → -10 [MW]

## BOP

**Pfusion** → 168 [MW]  
**Qfusion** → 22  
**thermal\_cycle\_type** → rankine  
**thermal\_efficiency\_plant** → 36.9 [%]  
**thermal\_efficiency\_cycle** → NaN [%]  
**power\_electric\_generated** → 63.1 [MW]  
**Pelectric\_net** → 38.4 [MW]  
**Qplant** → 2.56  
**TBR** → 1.1

SPARC  $P_{\text{fusion}} =$   
140 MW

## EXHAUST

**Psol** → 31.8 [MW]  
**PLH** → 25 [MW]  
**Bpol\_omp** → 1.15 [T]  
**λq** → 0.965 [mm]  
**qppl** → 1.21e+03 [MW/m<sup>2</sup>]  
**qpar** → 6.45e+03 [MW/m<sup>2</sup>]  
**P/R0** → 9.62 [MW/m]  
**PB/R0** → 75.6 [MW T/m]  
**PBp/R0** → 9.62 [MW T/m]  
**PBe/R0q95** → 4.83 [MW T/m]  
**neutrons\_peak** → 0.863 [MW/m<sup>2</sup>]

## BUILD

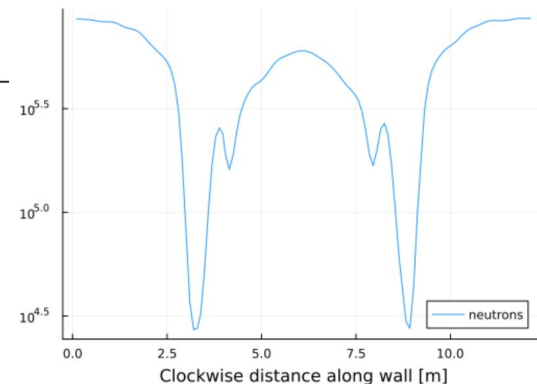
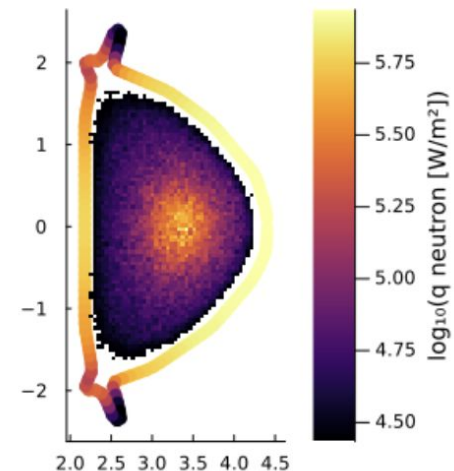
**PF\_material** → rebco  
**TF\_material** → rebco  
**OH\_material** → rebco  
**TF\_max\_b** → 16.4 [T]  
**OH\_max\_b** → 8.21 [T]  
**TF\_j\_margin** → 1.15  
**OH\_j\_margin** → 1.15  
**TF\_stress\_margin** → 1.15  
**OH\_stress\_margin** → 1.26

## CURRENTS

**ip\_bs\_aux\_ohm** → 7.52 [MA]  
**ip\_ni** → 2.51 [MA]  
**ip\_bs** → 2.26 [MA]  
**ip\_aux** → 0.253 [MA]  
**ip\_ohm** → 5.01 [MA]  
**ejima** → 0.4  
**flatop** → 0.105 [Hours]

## COSTING

**capital\_cost** → 5.44 [\$/B]  
**levelized\_CoE** → 2.05 [\$/kWh]  
**TF\_of\_total** → 10.5 [%]  
**BOP\_of\_total** → 3.98 [%]  
**blanket\_of\_total** → 3.2 [%]  
**cryostat\_of\_total** → 0.865 [%]





# Proposals for Collaboration DIII-D <> Maritime Fusion

(more are welcomed)

Focus Area	DIII-D Experiment	Relevance for Maritime Fusion
<b>Power-exhaust control (P_SOL, f_rad)</b>	20 MW NBI + 4 MW ECH, impurity seeding (Ne/N <sub>2</sub> /Ar), SAS divertor, f_rad ≈ 0.9 possible	Anchors radiative-mantle and detached operation needed for low-heat-flux Yinsen wall
<b>Edge/SOL similarity (<math>\lambda_q</math>, detachment)</b>	$\lambda_q \propto B_p^{-1}$ scaling accessible via Ip/q95 scans; SAS tungsten divertor for heat-flux mapping	Extrapolate $\lambda_q$ and detachment windows to Yinsen's high-B <sub>p</sub> regime
<b>ELM-free confinement (NT &amp; QH)</b>	Mature negative-triangularity and QH-mode; ELM-quiet plasmas at $\beta_N \approx 3-4$	Benchmarks pedestal structure and transport regime for Yinsen's steady, ELM-quiet flattops
<b>Tungsten compatibility</b>	First wall test section for W source/leakage studies at high f_rad	Demonstrates impurity screening and allowable Z_eff for compact devices
<b>High <math>\beta_N</math> confinement with benign wall loading</b>	$\beta_N$ up to ~5, strong shaping control ( $\kappa \approx 2$ , $\delta \pm 0.4$ ), dimensionless similarity scans ( $\rho^*$ , $v^*$ )	Validates achievable pressure & MHD stability limits for compact high-field reactor